and facsimile services has exploded. To keep pace with this technology and different system layout. The next section proexplosive demand, the wireless industry is currently launch- vides a detailed discussion of the two major PPI interference ing an aggressive campaign to deploy and operate an ever- mechanisms. PPI is disconcerting to wireless engineers for increasing number of wireless systems in a comparatively two reasons. First, unlike self-interference (brought about by small and modestly increasing sliver of spectrum. As an ex- frequency reuse), which usually occurs along the cell boundample, consider the broadband Personal Communications ary, PPI can occur anywhere in the victim PCS system's ser-Services (PCS) industry. As many as 2042 licenses are avail- vice area. Second, wireless engineers cannot easily predict or able for potential PCS service providers, and all these provid- mitigate PPI because the wireless engineer for one PCS sysers must operate their respective systems in only 120 MHz tem has no control over the design of the other PCS system. of spectrum. Moreover, each provider is free to choose any Therefore, most mitigation techniques that involve wireless technology. Currently, as many as eight technologies are system design and layout require some form of cooperation standardized for use in broadband PCS. Traditionally, wire- between competing PCS operators. The section entitled ''Inless system engineers focus on designing systems that provide terference Mitigation Techniques" presents a number of these a large subscriber base with an acceptably high Quality of techniques as well as equipment design approaches that Service (QOS) and Grade of Service (GOS) and operate in a should mitigate PPI. Recall that PPI is a consequence of the fixed spectrum allocation. To meet these spectrally con- different PCS systems and their varying emission limits and strained requirements, wireless engineers use combinations performance requirements. In the section entitled "IS-95," we of multiple access techniques and frequency reuse. Wireless discuss the performance requirements and emission specifiengineers use multiple access techniques to support parallel cations of one PCS technology, IS-95. We also discuss relevant transmission by subscribers over a fixed spectrum allocation. regulations that apply to the PPI issue. The subsection enti-Some common techniques include Frequency Division Multi- tled ''Interference Estimation Methodology'' presents an interple Access (FDMA), Time Division Multiple Access (TDMA), ference analysis methodology that shows how emissions from and Code Division Multiple Access (CDMA). one base station transmitter can cause excessive interference

any multiple access technique is not only finite but also a clusions are presented in the last section. function of available bandwidth (spectrum). Therefore, to further increase their system's spectral efficiency or available capacity, wireless engineers reuse frequencies in different re- **INTERFERENCE SOURCES IN WIRELESS COMMUNICATIONS** gions over the given service area. This technique, frequency reuse, provides a tradeoff between spectrum efficiency (or ca- In the design and analysis of any wireless system, engineers pacity) and interference. If a wireless engineer designs a sys- must consider a vast number of interference sources and tem with a high frequency reuse, the system will be spectrally mechanisms. These include various intrasystem interference efficient, thereby having a high GOS. However, the same ser- sources such as cochannel interference resulting from frevice will also be encumbered by excessive cochannel interfer- quency reuse, adjacent-channel interference and alternate ence, which will contribute to a low QOS. On the other hand, channel interference caused by the specific frequency plan if the same engineer reduces the frequency reuse, the sys- used in the system design, interference from spurious emistem's spectral efficiency will decrease, thus reducing the GOS. sions and other transceiver nonlinearities, and intermodula-However, the system's cochannel interference will decrease, tion interference from multicarrier transmission systems in thereby increasing the system's QOS. In any event, wireless base station transceivers. Also included are a number of inengineers can manage this particular form of self-interference tersystem interference sources, which are currently unique to via a prudent system design (i.e., selection of multiple access the PCS industry. These sources include cochannel interfertechnique, cell layout design, and frequency plan). In the sec- ence, adjacent channel interference resulting from the neartion entitled ''Intrasystem Interference,'' we discuss self-inter- far phenomenon, and intermodulation interference. ference and its relationship to various system design parame- To discuss all the interference mechanisms in wireless ters such as the frequency reuse factor and the frequency communications is beyond the scope of this paper. Rather,

censes in such a small spectral allocation imposes some generated, how they are related to relevant system design paunique challenges to wireless system engineers regarding in- rameters, and what overall effect they have on system perforterference management and mitigation. In the PCS industry, mance. With that in mind, we limit our discussion in the next up to six operators will provide service to the same service section to cochannel interference resulting from frequency rearea via adjacent frequency bands. Each operator may use use. In particular, we show the relationship between freany of eight standardized technologies, each with different quency reuse (or the frequency reuse factor) and the system emission characteristics and performance requirements. Fur- Carrier to Interference Ratio (CIR) requirement for acceptthermore, no coordination procedures exist between any oper- able QOS. Then we limit our discussion to two PPI mechaators that provide service to the same area. This potentially nisms—adjacent channel interference (due to the near-far dangerous situation increases the likelihood of a unique type phenomenon) and intermodulation interference—which may of interference called PCS-to-PCS Interference (PPI). PPI oc- occur when two or more PCS service providers colocate their curs when the in-band or out-of-band emissions of one (of- respective base station transceivers.

**COCHANNEL INTERFERENCE** fending) PCS system, with a given technology and system layout, interferes with receivers (usually mobile subscriber Over the past decade, the demand for wireless voice, data, receivers) of another (victim) PCS system with a different Regrettably, the number of transmissions supported by to nearby mobiles that subscribe to a competing service. Con-

reuse distance. this section discusses the major interference sources. In par-On the other hand, the proliferation of so many PCS li- ticular, we discuss how these interference mechanisms are

the capacity decreases and the cochannel interference decreases, thereby increasing QOS. Conversely, decreasing the reuse distance increases capacity at the expense of increased

and velocity of the mobile station. Generally, mobile stations an approximate value for CIR is given by that are located at the edge of a given cell receive a nominal carrier signal. Furthermore, these mobile stations also have a higher probability that the carrier signal is shadowed by some obstruction in the transmission path. Note that line of sight transmission is unlikely in such conditions. Therefore, mobile stations that reside at the fringe of a given cell have a  $\frac{1}{\sqrt{6D}}$ higher probability of receiving excessive cochannel interference than mobile stations residing in the cell's interior. If the mobile is moving at high speeds, the received carrier signal suffers from fast fading. Therefore, even though the CIR is Now consider the Advanced Mobile Phone System (AMPS)

use, capacity, and the system CIR requirement for acceptable using the canonical, single sector, hexagon grid model (Fig. 1). Furthermore, suppose that the provider implements a fre-



the reuse factor is seven. System.

# **COCHANNEL INTERFERENCE 513**

**Intrasystem Interference** *Intrasystem Interference neurouse scheme in the standard method by partitioning* Any wireless communication system that employs a frequency<br>reuse scheme is subject to cochannel interference. Indeed, comes set of frequencies. The provider then assigns these chan-<br>channel interference is the primary int

$$
D = R\sqrt{3N} \tag{1}
$$

interference, thereby degrading QOS.<br>Other factors that affect signal quality include the location the radius of the cell. Assuming a nath-loss exponent to be 4 the radius of the cell. Assuming a path-loss exponent to be 4,

$$
CIR = \frac{C}{\sum_{i=1}^{6} I_i}
$$
 (2)

$$
\approx \frac{R^{-4}}{6D^{-4}}\tag{3}
$$

$$
=1.5N^2\tag{4}
$$

under static conditions, it is large enough to maintain reliable wherein traffic modulation is based on analog Frequency communications. Under fading conditions, the CIR periodi- Modulation (FM). For a standard AMPS receiver (i.e., a stancally drops below the threshold required to maintain reliable dard Phased Lock Loop FM receiver) to reliably demodulate communication. Thus, wireless engineers generally add a fade a FM signal, thus providing toll-quality speech, the CIR must margin in the link budget to account for signal variations re- not fall below 63.09 (or 18 dB). Then a cluster size of seven sulting from fading and shadowing. will provide sufficient protection from cochannel interference To illustrate the basic relationships between frequency re- so that a CIR of 18 dB is maintained. This results in a frequency reuse factor of  $\frac{1}{7}$ . Furthermore, suppose that a cellular QOS, consider the following example. Suppose a wireless ser-<br>vice provider designs an AMPS-based system in such a<br>vice provider (cellular, PCS, or otherwise) with an allocation manner that it consists of 42 cells and has s vice provider (cellular, PCS, or otherwise) with an allocation manner that it consists of 42 cells and has sufficient spectrum of M channels deploys a system over the given service area to accommodate 21 duplex channels. T to accommodate 21 duplex channels. Then with a frequency reuse of  $\frac{1}{7}$ , the provider can assign the same channel to every seventh cell. Thus, the provider assigns three channels to each cell. If we assume that no channels are used for signaling or control purposes, this wireless system can support a capacity of 126.

Suppose however, that by using some interference mitigation techniques (e.g., interference cancellation), a manufacturer designs an interference-resistant AMPS-compliant receiver that reliably demodulates the FM signal when the  $CIR = 8$  (or 9.03 dB). Then a cluster size of three will provide sufficient protection from cochannel interference. This results in an increased frequency reuse factor of  $\frac{1}{3}$  and an increase in capacity that exceeds a factor of 2. Indeed, in this example, with an increased frequency reuse of  $\frac{1}{3}$ , the provider can assign each cell seven channels rather than three. Hence, the available capacity increases from 126 to 294. Note that if one designed an interference-resistant receiver that operated with a CIR of 1.5 (or 1.76 dB), wireless systems with a frequency reuse of 1 would then be possible. A CDMA system such as Figure 1. Cochannel problem in a typical cellular environment. Here IS-95 with its Rake receiver design is an example of such a

### **514 COCHANNEL INTERFERENCE**

The steered of Newsale Conventions Serves to the single Party and the single entroid in t

ence generally affects the mobile receiver. Moreover, this form holes, depending on their location, will result in customer dis-

**Intersystem Interference** of interference is a consequence of the near-far phenomenon.

nel interference from other service providers' base stations **Adjacent Channel Interference.** Adjacent channel interfer- will create coverage holes in a given network. These coverage satisfaction, loss of customers, loss of revenue, and loss of **INTERFERENCE MITIGATION TECHNIQUES** profitability. Therefore, the existence, location, and size of these coverage holes can have a direct and adverse impact on In the initial phase of a cellular network deployment, capacity the financial performance of the given network. is not an issue, and hence a cellular service provider designs

of another transceiver. The presence of the leaked signal will minimized by carefully designing the system (e.g., sectoriza-<br>cause the power amplifier (a nonlinear device) to produce in-<br>tion channel allocation etc.) or by cause the power amplifier (a nonlinear device) to produce in-<br>tion, channel allocation, etc.) or by implementing interference<br>termodulation interference into the corresponding receive<br>mitiration techniques based on signal channels of some of the transceivers on the tower. A common ceiver. example of the latter case is the interaction of two or more transmitted signals and a rusty bolt on a tower. Such an in- **Sectorization**

Specialized Mobile Radio (SMR) provider. However, because<br>cellular and SMR providers implemented common, narrow<br>band technologies, they could easily resolve interference cases<br>by moving one or more of the frequency assignm

The effect of intermodulation interference is illustrated in the following example. Suppose a customer in Blacksburg, Virginia, has enjoyed a high quality of service from his PCS service for the past 12 months. This particular customer travels only in and around Blacksburg. Therefore, he rarely leaves the coverage area of the three sectors operating on the one tower in Blacksburg. However, last week he noticed that his calls were being interrupted, and the interruption in service was becoming more consistent. What particularly bothered the customer was that the voice quality of the other party was exceptional (indicating that there was no interference in the downlink). Nevertheless, frustrated with the consistent interruptions in service, the customer cancelled his PCS service and subscribed to a competing PCS service, which went into operation about a week ago. Coincidentally, the competing PCS service provider operates its service in that area on the same tower.

The customer in question was a victim of intermodulation interference. This particular form of interference affects only the uplink. Therefore, the sector serving the customer could not clearly receive the signal from the customers mobile station, even though the customer could receive the signal from the sector. Because the sector in question was unable to receive the signal after as many as 64 attempts, the PCS system dropped the call. Such interference events will affect the network by causing large holes in the uplink coverage. These holes will adversely affect call quality and grade of service. (b) This has a direct and deleterious impact on system capacity, **Figure 2.** Sectorization in a typical cellular system: (a) 120° sectorisubscriber satisfaction, and network revenue.<br>zation and (b) 60° sectorization. subscriber satisfaction, and network revenue.

the network to maximize coverage. Base stations are sited to Intermodulation Interference. Intermodulation interference<br>
is a common problem in situations where many transceivers<br>
operate at the same location (e.g., on a radio tower). This form<br>
of interference is a consequence of t mitigation techniques based on signal processing at the re-

teraction will produce intermodulation interference into the<br>corresponding receive channels of some of the transceivers on<br>that tower.<br>Intermodulation interference is not unique to the PCS in-<br>directional antennas, each ra



### **516 COCHANNEL INTERFERENCE**

 $120^{\circ}$  sectorization is employed, the number of interferers is GHz) with existing microwave systems, the addition of a vast reduced to two. number of new low-earth-orbiting (LEO) satellites with over-

of 12 is required to maintain a CIR of 18 dB. However, with of high definition television (HDTV) transmissions within the 120° sectorization, a CIR of 18 dB can be achieved with a current TV band. reuse factor of 7. Thus, sectorization reduces interference, which can be translated into an increase in capacity by ap-<br>**Adaptive Interference Rejection.** Interference rejection techproximately  $\frac{12}{7}$ . In practice, the reduction in interference offered by sectoring enables cell planners to reduce the cluster ture of interference and the channel. Methods of interference size and provides additional degrees of freedom in assigning rejection can be viewed as adaptive filtering techniques. The channels. The penalty for improved CIR and the resulting im- term *filter* is often used to describe a device (software or hardproved capacity is an increase in the number of antennas and ware) that is applied to a set of corrupted data to extract ina decrease in trunking efficiency as a result of channel sec- formation about a prescribed quantity of interest. The design toring at the base station.  $\Box$  of an optimum filter requires a priori information about the

lar capacity is inherently interference limited, particularly by In the past, capacity enhancement using adaptive arrays for cochannel interference (CCI) and adjacent channel interfer- land mobile radio systems have been investigated (2,3). Adapence (ACI). One solution to combat CCI and ACI is to split tive arrays have been investigated for CDMA (4,5), TDMA cells and decrease power, but cell splitting is expensive. Inter- (6,7), and FDMA (8,9) systems to mitigate cochannel interferference rejection techniques often represent a less-expensive ence and multipath components. Capacity increase provided alternative to cell splitting. by adaptive arrays for CDMA systems have been investigated

In addition, as newer communication technologies super- in the past  $(10-12)$ . sede older technologies, interference rejection techniques are important in helping to facilitate compatibility during transi- **Spread Spectrum versus Nonspread Spectrum.** Spread spections between the old and new technologies. Several examples trum (SS) is by nature an interference tolerant modulation. illustrate the need for compatibility: coutilization of the ex- However, there are situations where the processing gain is isting cellular band with new narrow band CDMA and TDMA inadequate, and interference rejection techniques must be digital cellular signals, design of broadband CDMA over- employed. This is especially true for direct sequence spread laying AMPS signals in the cellular bands, coutilization of the spectrum (DS-SS), which suffers from the near-far problem.

the number of interferers in the first tier is six, but when new personal communication system band (1.8 GHz to 2.2 When the mobile is at the edge of the cell, a reuse factor lapping footprints with older satellites, and accommodation

niques often need to be adaptive because of the dynamic nastatistics of the data to be processed. Where complete knowl-**Channel Allocation** edge of the relevant signal characteristics is not available, an For effective use of the radio spectrum, a frequency reuse adaptive filter is needed. This filter is a self-designing device<br>scheme that is consistent with the objectives of increasing the<br>capacity and minimizing the inter

cochannel interference can be reduced. If the old channel is single-Channel versus Multichannel. Single-channel adap-<br>suffer from interference can be reduced. If the old channel is two filtering techniques are interferenc

ploying a spatial filter at the base station. SDMA exploits spa- **Signal Processing Techniques** tial diversity, and it increases the signal to interference ratio Interference rejection is important for several reasons. Cellu- by spatially isolating the desired user from the interference.



**Figure 3.** Classification of single-channel interference rejection techniques.

SS categories include direct sequence (DS), CDMA, and fre- **INTERFERENCE ISSUES** quency hopping (FH).

techniques and (2) those based upon transform domain pro- sues can be classified as cessing structures. The improvement achieved by these techniques is subject to the constraint that the interference be • Transmitter output, relatively narrow band with respect to the DS waveform. Poor  $\cdot$  Channel planning, and Rusch (14,15) give an overview of narrowband interfer- $\cdot$ , Transmit/ressive d and Rusch (14,15) give an overview of narrowband interfer-<br>ence suppression in SS CDMA. They categorize CDMA inter-<br>ference suppression by linear techniques, nonlinear estima-<br>tion techniques, and multiuser detection techn

lation receivers that correlate the received signal with a **FCC Regulations** synchronized copy of the desired signal's spreading code. Conventional receivers treat multiple access interference (MAI), The FCC Rules (17) and the FCC Memorandum (18) state chronous mode, and hence the orthogonality of the codes is corresponding decrease in the radiated power. These requireno longer beneficial. Therefore multiuser rejection techniques ments are listed in Table 1. have been developed to use the knowledge of all the users' Mobile or portable stations are limited to 2 W EIRP peak

Several tutorial papers have been published on interfer- This section focuses on transceiver issues and FCC regulaence rejection in SS, and Milstein's paper (13) is of particular tions to reduce interference in the licensed PCS bands. The interest. Milstein discusses in depth two classes of rejection interference problem is enhanced by coexisting multiple stanschemes (both of which implement an adaptive notch filter): dards, which can interfere with each other and make the in- (1) those based upon least mean square (LMS) estimation terference analysis much more complicated. The receiver is-

- 
- 
- 
- 
- 

detailed survey of different signal-processing techniques can<br>be found in Ref. 16.<br>A classification of wideband interference rejection tech-<br>niques for direct sequence CDMA is shown in Fig. 4. The cur-<br>rent generation of C

which is inherent to CDMA, as additive noise. In the down- that the base stations are limited to 1640 W peak equivalent link, the orthogonality of the codes helps mitigate mutual in- isotropically radiated power (EIRP) with an antenna height terference. But in the uplink, the users are operating in asyn- of 300 m. Base station heights may exceed 300 m but with a

codes at the base station to reject interference. power, and the equipment must employ means to limit the



**Figure 4.** Classification of wideband interference rejection techniques for direct sequence CDMA systems.

the base station. Therefore, the taller the antennas, the less fundamental emission of the transmitter shall be employed. power they are allowed to transmit. There is a tradeoff be- The transmitter output power of the base station in any tween the coverage of and the amount of interference emitted 1.25 MHz band of the base station's transmit band between by a certain base station. The antenna height must be de- 1930 and 1990 MHz and in any direction shall not exceed 100 signed to reduce the amount of interference to the neigh- W. For all the frequencies within the band 1930 MHz to 1990 boring base stations. MHz, the total conducted spurious emissions in any 30 kHz

power to the minimum necessary for successful communica- not exceed  $-13$  dBm outside the band of interest. The resolutions. On any frequency outside the licensee's frequency tion bandwidth for measuring these emissions shall be 1 block, the power of any emission shall be attenuated below MHz, except within the 1 MHz bandwidth immediately outthe transmitter power *P* by at least  $43 + 10 \log P$  dB. The side and adjacent to the frequency block, where the resolution antenna height at the base station dictates the coverage of bandwidth of at least 1% of the emission bandwidth of the

band greater than 885 kHz from the CDMA center channel **IS-95** frequency shall not exceed a level of  $-45$  dBc.

This subsection deals with the receiver issues for IS-95 sys-<br>tems. The following FCC requirements are extracted from<br>Refs. 19–21).<br>Refs. 19–21).

**Power Characteristics for Base Station and the Mobile.** The **Channel Spacing.** The channel assignments for the mobile FCC also regulates spurious emissions outside the band of interest to minimize adjacent channel interfe are conditionally valid. Transmission on conditionally valid channels is permissible if the adjacent block is allocated to

**Table 1. Reduction in Power for Antenna Heights over 300 m**

Height(m)	Maximum EIRP (W)
$\leq$ = 300	1,640
$\leq$ =500	1,070
$\leq$ = 1,000	490
$\leq$ = 1,500	270
$\leq = 2,000$	160

**Table 2. Spurious Emissions Limits**



**Table 3. Channel Assignments**

Transmitter	CDMA Channel Number	Center Frequency of CDMA Channel (MHz)
Mobile	$0 \le N \le 1199$	$1850.00 + 0.050N$
Base	$0 \le N \le 1199$	$1930.00 + 0.050N$

the licensee or if other valid authorization has been obtained.<br>
Also the base station transmit carrier frequency shall be B base,<br>  $\frac{B}{B}$  base,<br>  $\frac{C}{B}$  base,<br>  $\frac{D}{C}$  and  $\frac{E}{D}$  a  $\frac{D}{C}$  and  $\frac{E}{D}$  are t ment. The mobile transmit carrier frequency shall be below<br>the base station transmit frequency, as measured at the mobile,<br>bile, by 80 MHz  $\pm$  150 Hz.<br> $\cdot$  Technology B mobile transmitter impacting a Technology<br> $\cdot$  Tech

duty cycle decide the amount of cochannel interference contributed by any user. In a IS-95 system, when operating in a<br>variable data rate transmission mode, the mobile transmits power, antenna height, and feeder losses. Third-order invariable data rate transmission mode, the mobile transmits power, antenna height, and feeder losses. Third-order in-<br>at nominal controlled power levels only during gated-on peri-<br>termod products, multiple interferens, cohe ods, each defined as a power control group. The time response and antenna radiation pattern are not included. of the ensemble average of power control groups, all with the To analyze the amount of interference, the metric used is same mean output power, shall be within the limits in Fig. the *degradation in receiver sensitivity* also called *receiver de-*5. During the gated-off periods, between the transmissions of *sensitization* and the threshold for impact when the interferpower control groups, the mobile shall reduce its mean output ence power plus the existing thermal noise plus the in-system power by at least 20 dB either with respect to the mean out- interference power is 3 dB above the original interference put power of the most recent power control group or to the plus thermal noise power. For example, a 3 dB receiver desentransmitter noise floor, whichever is greatest. sitization reduces the effective system range and reduces the

eled using a two-slope path loss model (24) as **Transmitter Intermodulation.** Spurious intermodulation products are produced whenever frequency signals mix in nonlinear RF stages. In particular, transmitter final stages tend to be quite nonlinear, with the presence of at least one strong signal guaranteed. Other signals may be picked up by the antenna and transferred to these stages with subsequent retransmission of the resulting spurious intermodulation products. The main concern is usually the third-order intermodulation products because resulting intermodulation products can fall on nearby frequencies of interest. In-band trans-<br>
mitter intermodulation generation will generally be of greater<br>
concern than in-band sideband noise, as the latter is of much<br>
less power compared to the fo



trol group). The mass of the m

### **Interference Estimation Methodology**

The methodology used here is adopted from References 22 and 23. Here the T-R separation, for which the spurious emissions from the transmitter (at maximum power because the mobile is assumed to be at the cell edge) of one technology would impact the receiver of the other technology, is estimated using simple path-loss calculations. Interference between four transmitter/receiver pairs are analyzed:

- 
- 
- A base, and
- **Figure 1)** Transmit **/ Receive Duty Cycle.** The transmit and the receive A mobile.

termod products, multiple interferers, coherent interference,

cell size by 15% to 30%. The propagation environment is mod-

$$
r_{\rm t} = \frac{4h_{\rm b}h_{\rm m}}{\lambda}
$$
  
Path loss =  $\left(\frac{4\pi r}{\lambda}\right)^2$ ,  $r \le r_{\rm t}$  (5)

Path loss = 
$$
\left(\frac{4\pi r^2}{\lambda r_t}\right)^2
$$
,  $r > r_t$  (6)

### **Calculation of Interference Distance versus Receiver Desensitization**

The following calculation is extracted from Ref. 25. The procedure to calculate the interference distance as a function of receiver desensitization follows.

In Ref. 25, the following parameters are defined:

- $N_i$ ,  $n_i$ —original interference density (dBm/Hz)  $(n_i$  in mW/ Hz),
- NF—receiver noise figure (dB),
- $(N_o, n_o$ —thermal noise density (dBm/Hz)  $(n_o$  in mW/Hz),
- **Figure 5.** Transmission envelope mask (average gated-on power con-<br>  $\mathbf{v}(N_e, n_e$ —out-of-band emission density (dBm/Hz) ( $n_e$  in mV/Hz).

# **520 COCHANNEL INTERFERENCE**

All the summations in the following discussion are done in **CONCLUSIONS** milliwatts per hertz, not in decibel-watts per hertz.

$$
D = 10 \times \log_{10} \left[ \frac{(n_e + n_i + n_o)}{(n_i + n_o)} \right] \, \text{dB} \tag{7}
$$

raise their power to maintain the required  $E_o/N_t$  where  $N_t = n_i + n_o + n_e$ . Thus *D* will also depend on the number of active

$$
D = 10 \times \log_{10} \left[ \frac{n_e + n_o}{n_o} \right] \, \text{dB} \tag{8}
$$

# **Procedure.**

- 
- 2. Find the path loss (PL) for the calculated  $N_e$  using the manuscript. following expression. The emission power spectral density (received at the receiver antennas port of the re- **BIBLIOGRAPHY** ceiver module) can be expressed as

$$
PL = P_{tx} - L_{tx} + G_{tx} + E_{msk}(\Delta f) - 10 \times log_{10}(RBW)
$$

$$
- N_e + G_{rx} - L_{rx} dBm/Hz
$$

- 
- $\Delta f$  is the offset frequency of the emission relative to the<br>carrier frequency,<br>carrier frequency,<br>the emission relative to the<br>5. T. Nagayasu and S. Sampei, Elimination of adjacent channel in-<br>terference via nonlinear f
- $E_{\text{msk}}$  is the Emission mask specification at  $\Delta f$ ,  $\Delta f$

*IEEE Trans. Commun.,* **42**: 1740–1751, 1994. 3. Calculate the cell radius *r* using Step 2 and using the propagation formula in Eqs.  $(5)$  and  $(6)$ . 8. P. Petrus and J. H. Reed, AMPS cochannel interference rejection

This methodology can be used to design systems with mini-<br>
9. P. Petrus and J. H. Reed, Time dependent adaptive arrays, *IEEE* mal interference. Therefore, the separation between base sta-<br>tions can be determined using this approach. The distance<br> $\frac{Sig}{\Delta E}$  Nagnih A Paulrai and T Kai tions can be determined using this approach. The distance 10. A. F. Naguib, A. Paulraj, and T. Kailath, Capacity improvement between the base stations is dependent on the path loss model of base-station antenna arrays in c being used. The two-slope path loss model may not be the *lomar Conf.,* 1993, pp. 1437–1441. appropriate model for many environments. Hence site-specific 11. A. F. Naguib, A. Paulraj, and T. Kailath, Capacity improvement propagation tools can be used to determine path loss in any with base-station antenna arrays in cellular CDMA, *IEEE Trans.* given geographical region. *Veh. Technol.,* **43**: 691–697, 1994.

In this article we addressed interference issues in wireless **Desensitization (D) for TDMA Systems (PCS1900, IS-136) and** communications systems. Interference issues are an increas-<br>**CDMA Systems (IS-95).** Desensitization for TDMA systems is tems face more interference related chall existing wireless systems because of the coexistence of different signal standards. Systems with measures to counteract  $\frac{1}{2}$  interference are deployed to increase the signal-to-interference plus noise ratio and to improve capacity. Most of the future wireless systems will have some type of signal-pro-Here we need to know  $(n_e + n_i + n_o)/(n_i + n_o)$ . cessing-based interference mitigation technique.

For CDMA systems, *D* is defined in a different way because In practice, other issues determine the capacity of a syspower control is employed in these systems. In IS-95 if there tem. The margin in the link budget given for fading can reis extra interference, all the mobiles in the cell/sector will duce the system capacity. If an adaptive signal-processing technique is employed at the receiver to combat interference as well as fading, the system performance will improve. For mobile units. For ten mobiles, the desensitization is close to example, if there are multiple antennas at the base station, signals at different antennas can be combined, fading effects can be mitigated, and interference rejection can be used.

# **ACKNOWLEDGMENTS**

The authors acknowledge Bob Boyle for helping us improve 1. Given *D* in decibels, the corresponding  $N_e$  is calculated Monica Maheswari of Mobile and Portable Radio Research using Eq. (7) or (8). Group, Virginia Tech, for their help in the preparation of the

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	-
- RBW is the resolution bandwidth (Hz), 6. J. H. Winters, Signal acquisition and tracking with adaptive PL is the required path loss (dB), arrays in the digital mobile radio system IS-54 with flat fading,<br>  $G_{rx}$  is the Rx antenna gain (dB),  $EEE Trans. Veh. Technol., **VT-42**: 377–384, 1993.$ <br>  $T. J. H. Winters, J. Salz, and R. D. Gitting in the impact of antenna  
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**CODE DIVISION MULTIPLE ACCESS 521**

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